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Title: QAM Multi-path Characterization Due to Ocean Scattering

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QAM Multi-path Characterization Due to Ocean Scattering

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Abstract

A series of RF channel flight characterization tests are to be run, in early March, to benchmark high speed, 16QAM multi-path performance over the ocean surface. The modulation format being tested is a 16 differential phase, absolute amplitude, two level polar quadrature amplitude modulation. The bit rate is 100 Megabits per second. This transmitted signal will be generated in a burst mode, being on for 40 microseconds once every 40 milliseconds. An aircraft will radiate the RF test signal at 5 different altitudes. The aircraft will make two inward flights at each altitude with vertical and horizontal polarization respectively. Receivers are to be placed in two different locations using circular antenna polarization. One receiver will be placed at an altitude of 230 feet above the ocean surface, and the other on a boat with the antenna placed just up off of the ocean surface. Data is to be collected over multiple wavelength changes in the difference between the line of sight and the reflected multi-path ray. The real time signal strength variation is to be recorded as well. Analysis of the resulting data will show flat fading and frequency selective fading effects. The test is run over two different days to provide for some variation in sea state conditions. This resulting information will help quantify the effectiveness of this novel modulation scheme for missile telemetry end event data applications.

QAM Multi-path Characterization Due to Ocean Scattering

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Roger Bracht

Authors:

Richard Swanson, Jeff Dimsdile

Honeywell Federal Manufacturing & Technologies

Tom Petersen, Regina Pasquale, Roger Bracht

Los Alamos National laboratory

Presentation to ITC 2002

San Diego, CA

October 22, 2002

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Aircraft Test Description

Transmitted from aircraft at 5 altitudes

Horizontal and Vertical polarizations

One receiver at Point Sur Lighthouse 230' above sea level

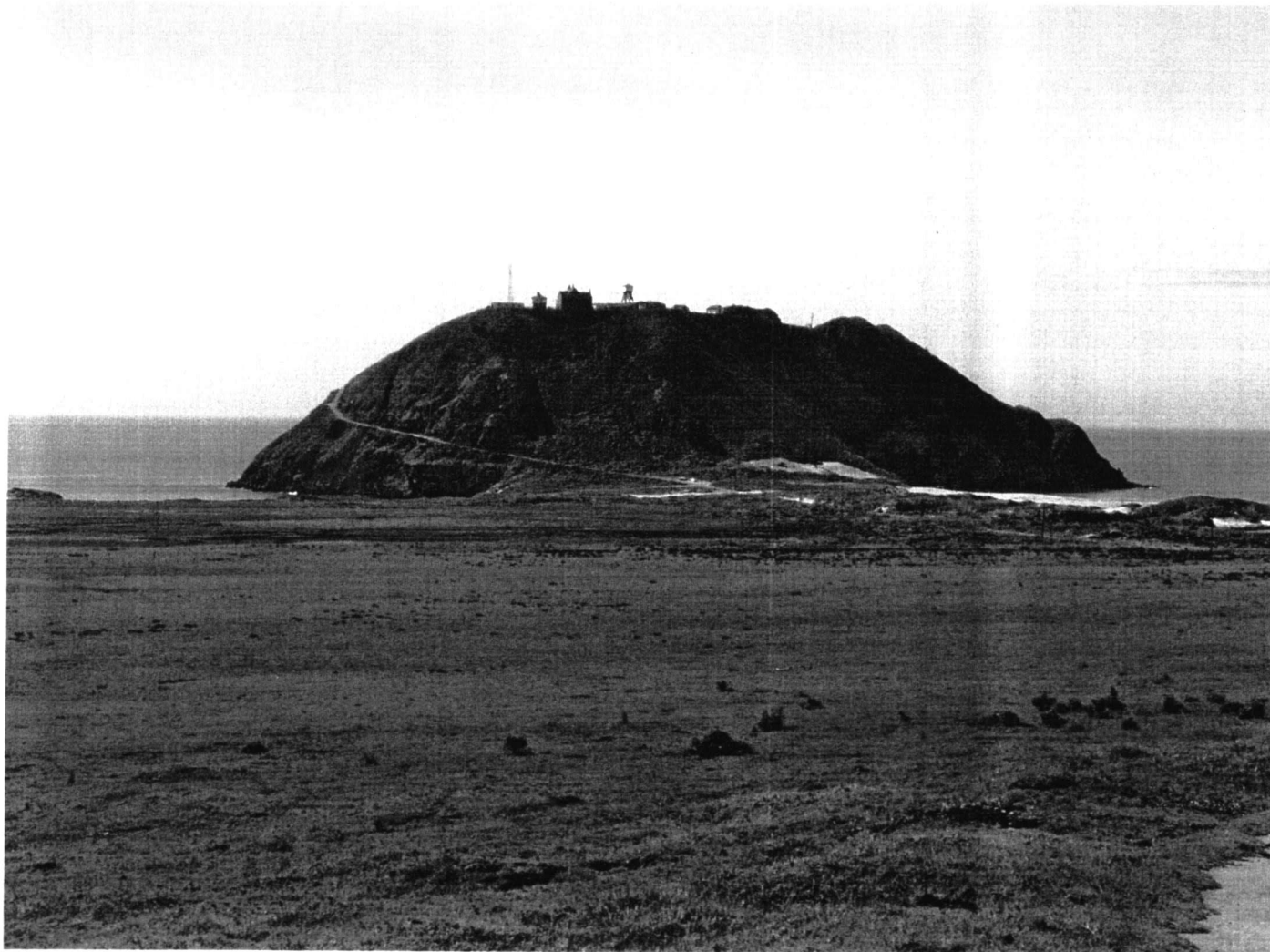
Other receiver on a boat with antenna just above the ocean surface

Two separate test days: Tuesday very calm seas, Friday fairly rough seas

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Pt. Sur



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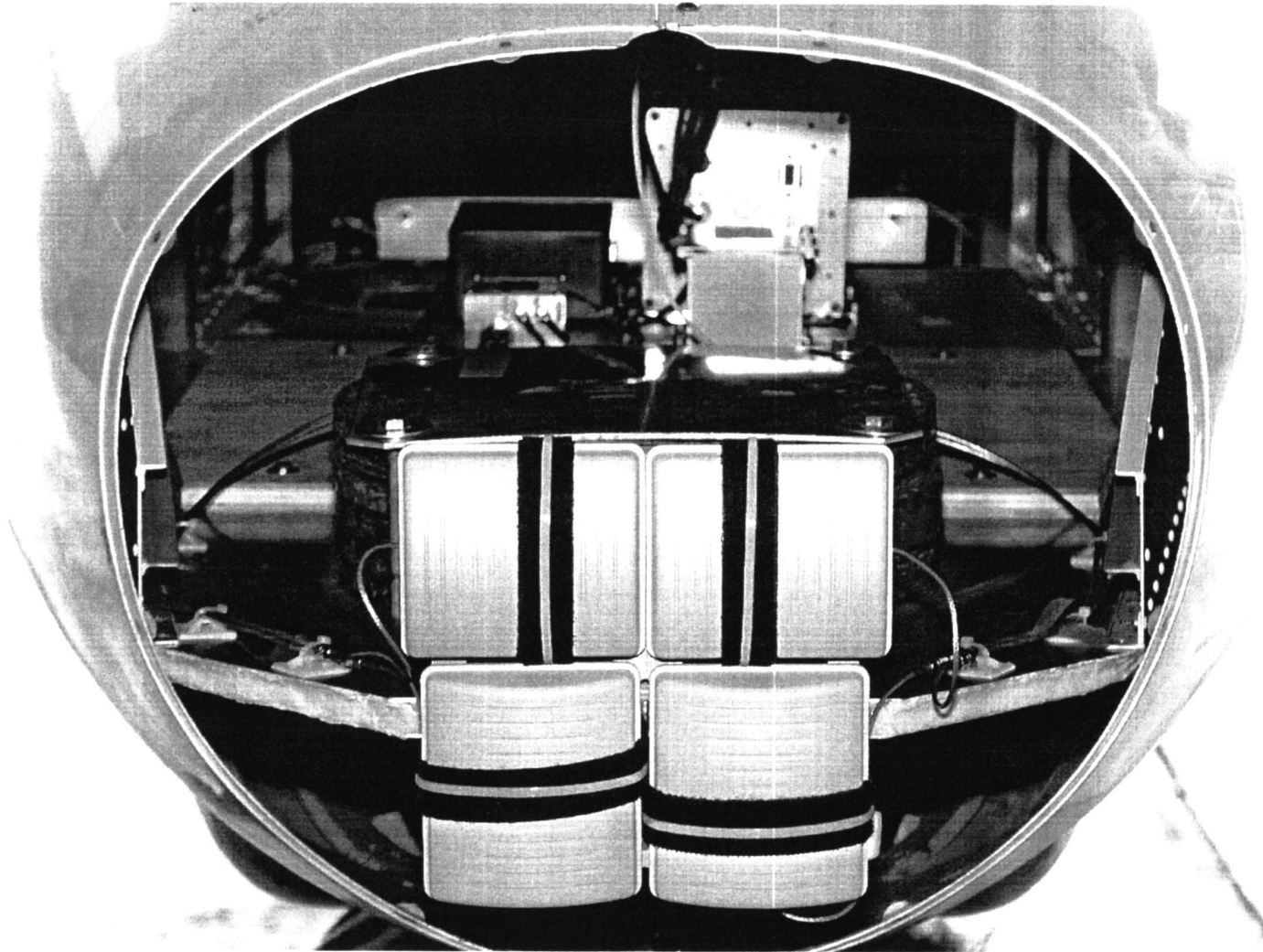
Pelican Aircraft



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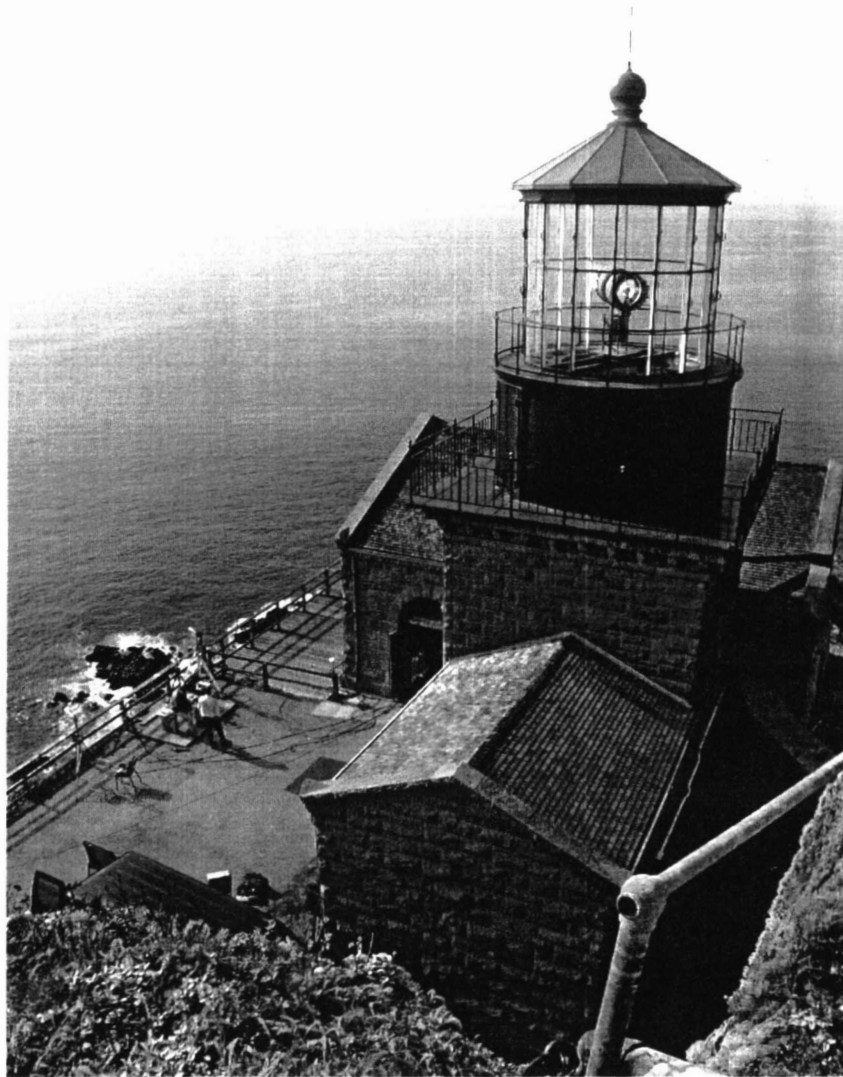
FQPSK, HERT, and Antennas



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Pt. Sur Light House



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Antenna Farm



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Buoy Simulator



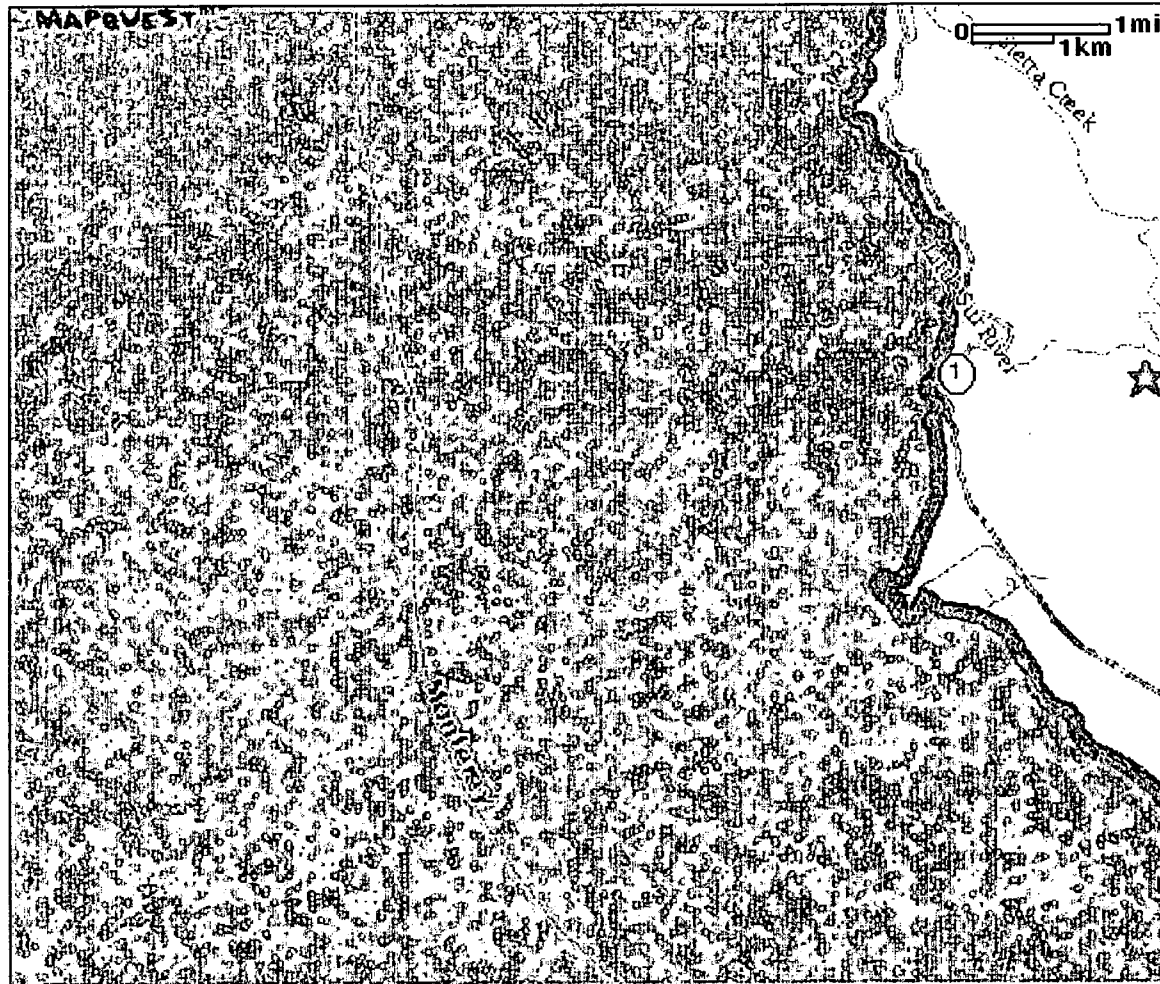
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Testing



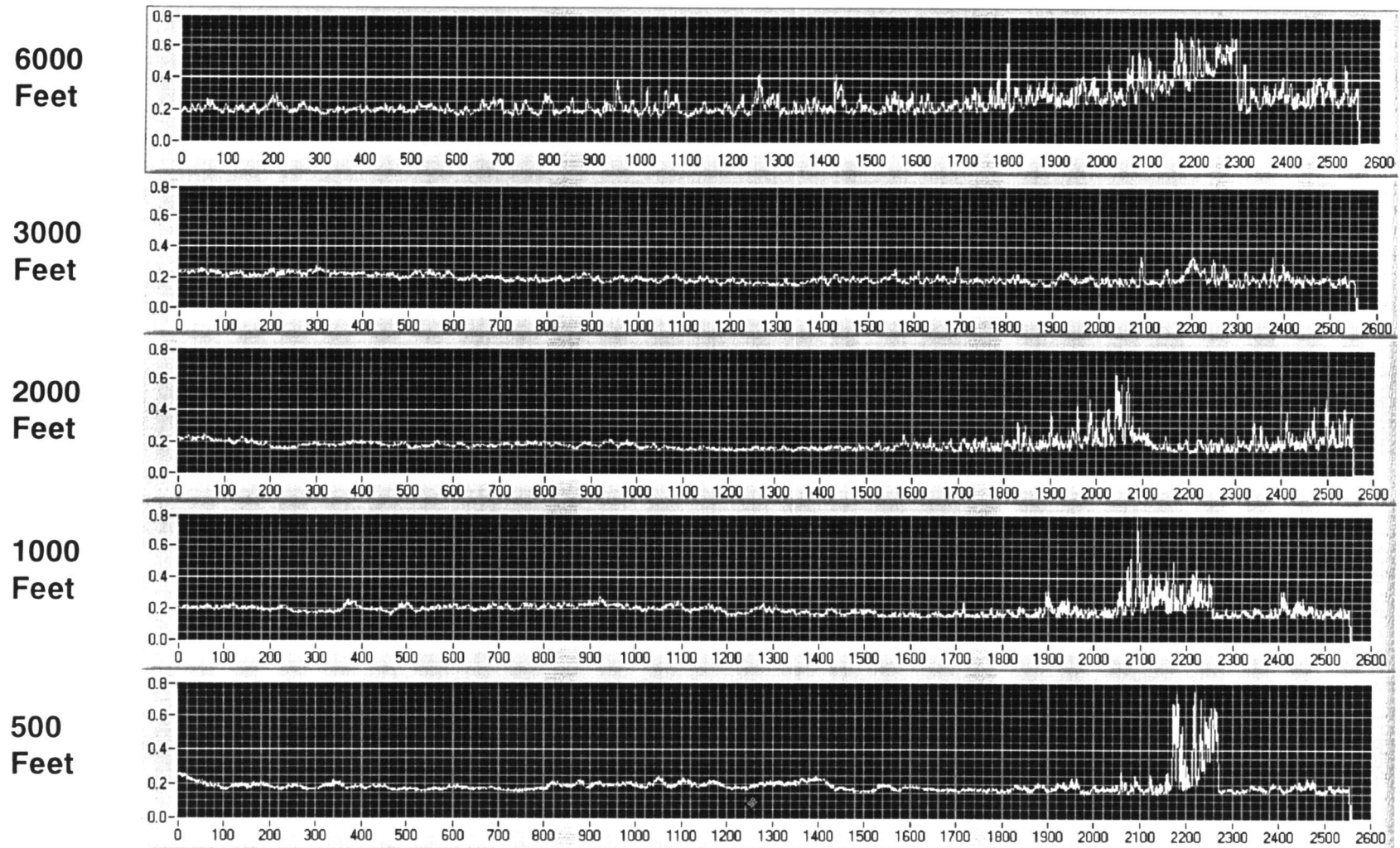
Pt. Sur



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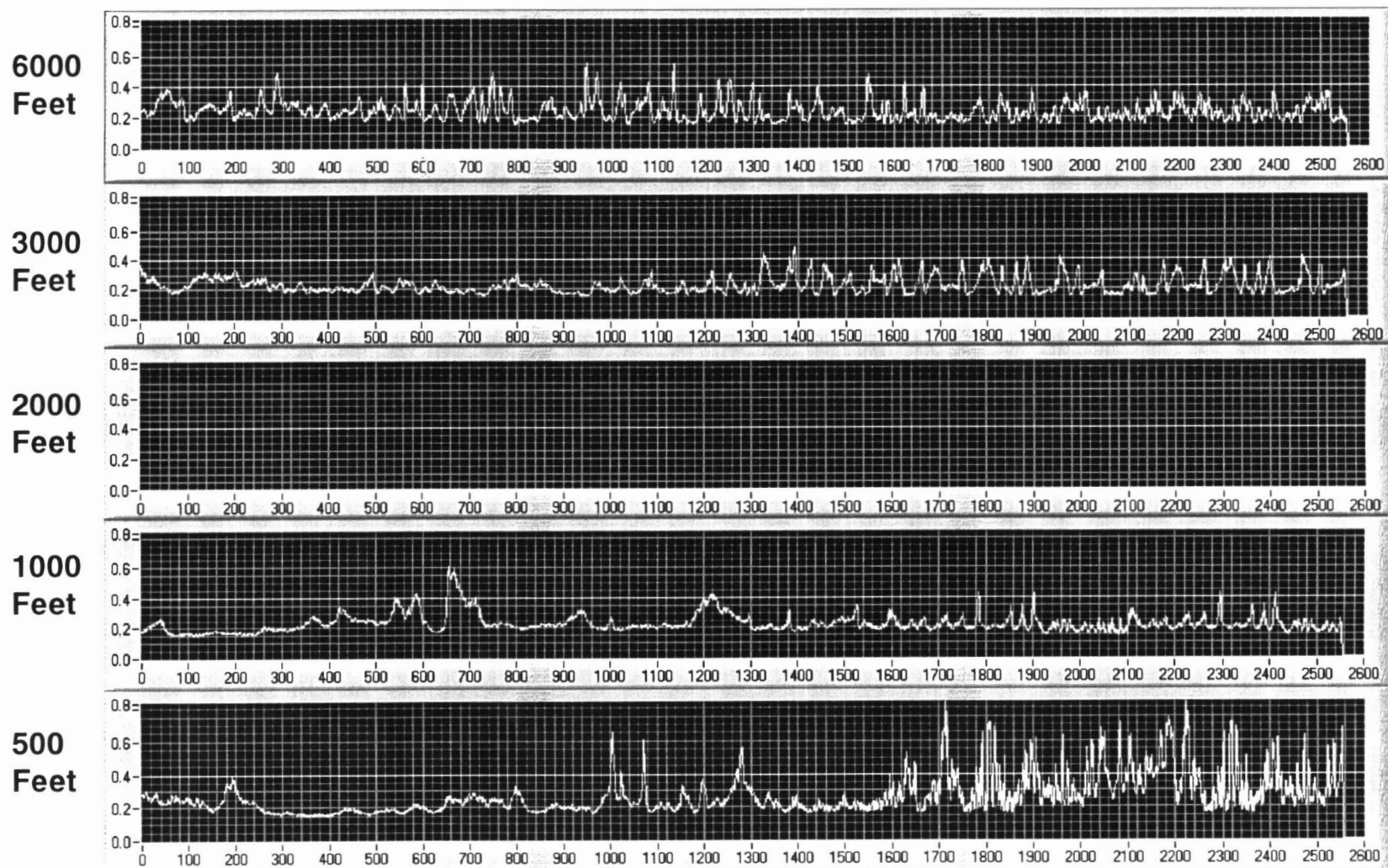
Calm Water Airplane to Boat with Vertical Radiator - QAM Deviation Spreads



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Calm Water Airplane to Boat with Horizontal Radiator - QAM Deviation Spreads

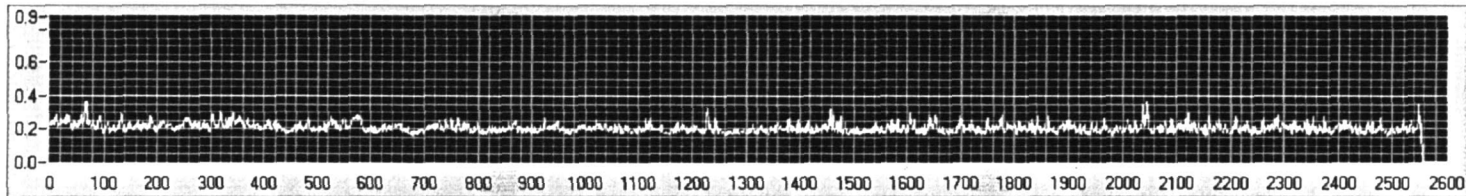


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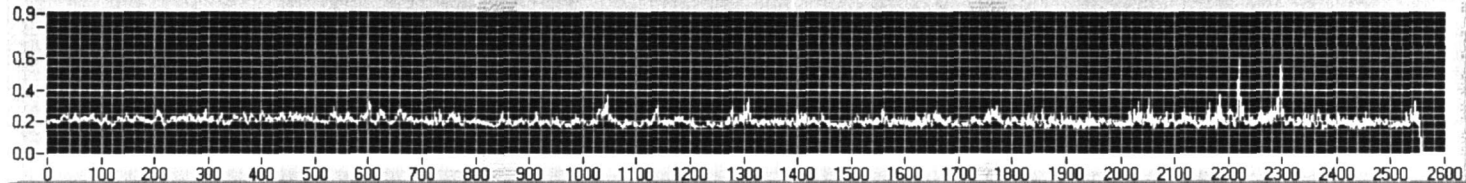
 **Los Alamos**

Rough Water Airplane to Boat with Vertical Radiator - QAM Deviation Spreads

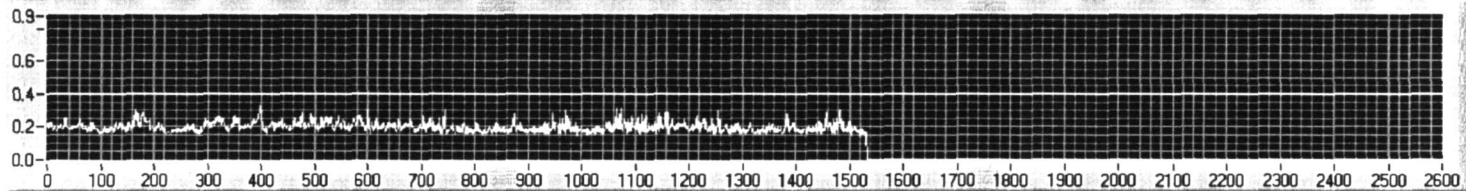
6000
Feet



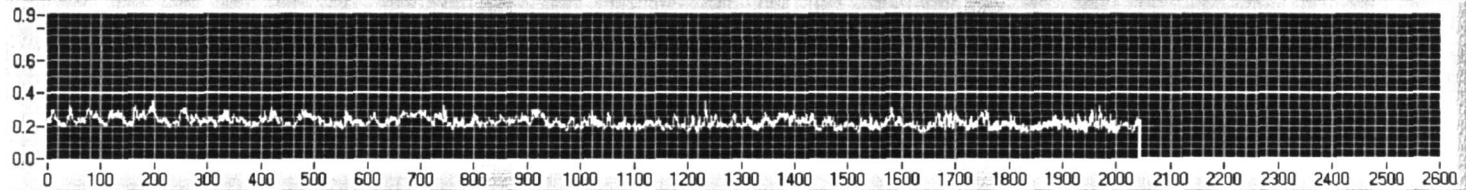
3000
Feet



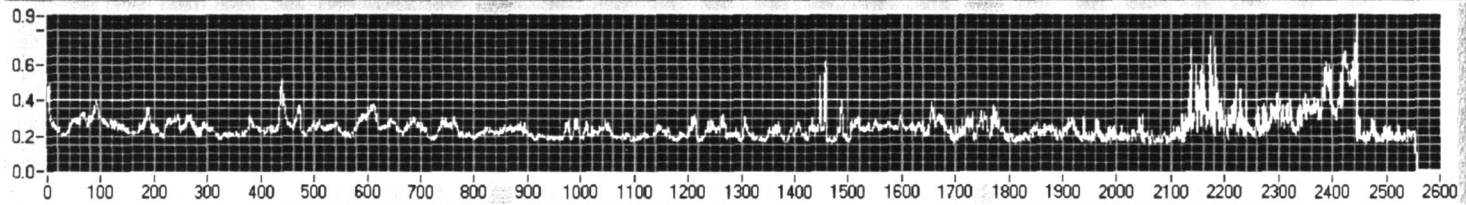
2000
Feet



1000
Feet



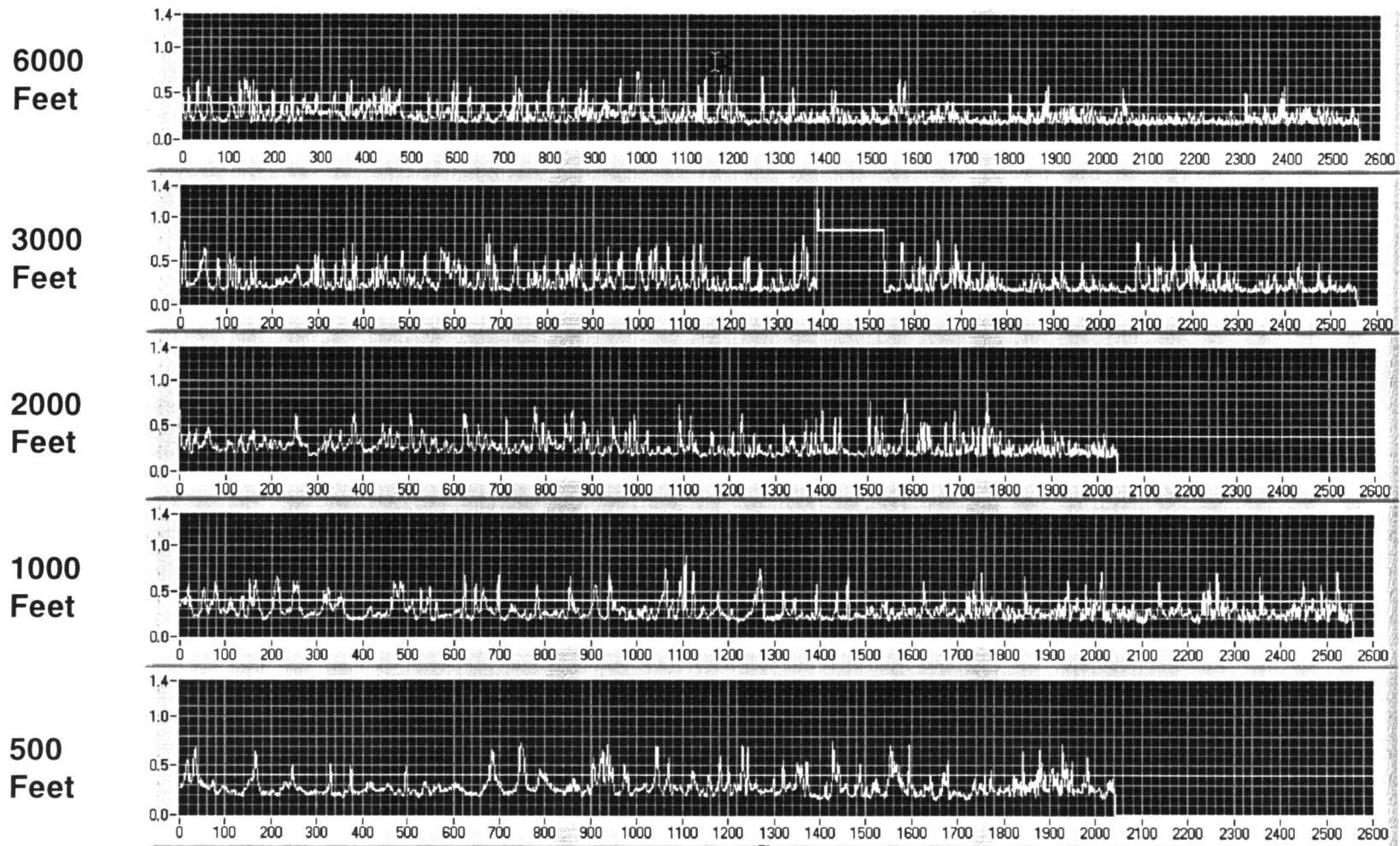
500
Feet



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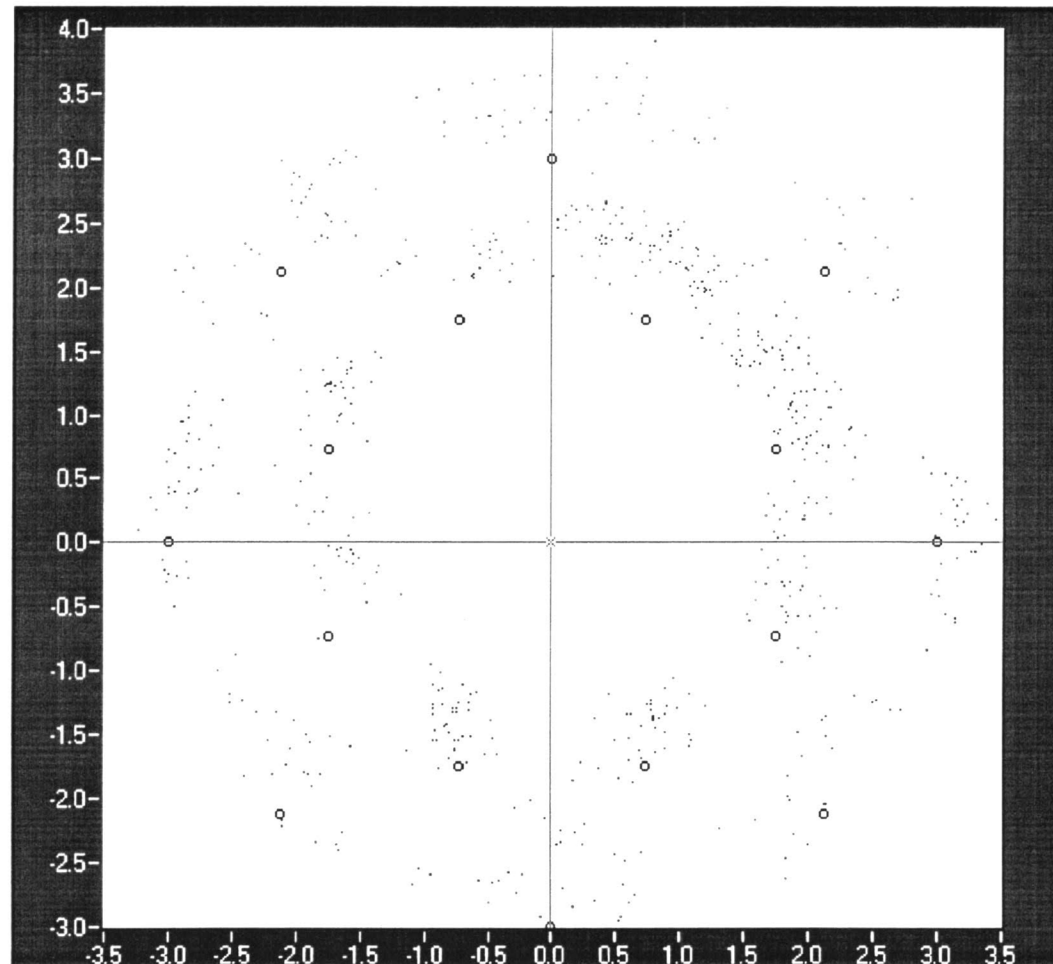
Rough Water Airplane to Boat with Horizontal Radiator - QAM Deviation Spreads



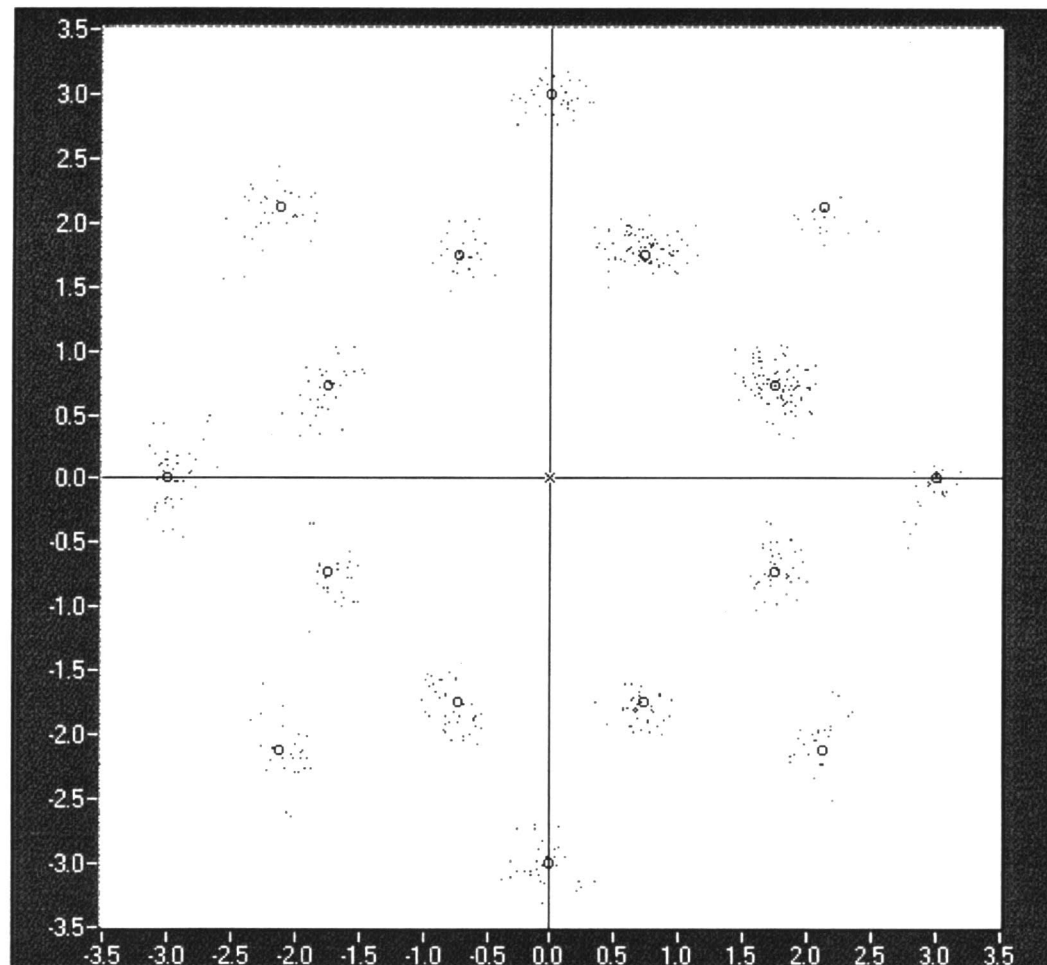
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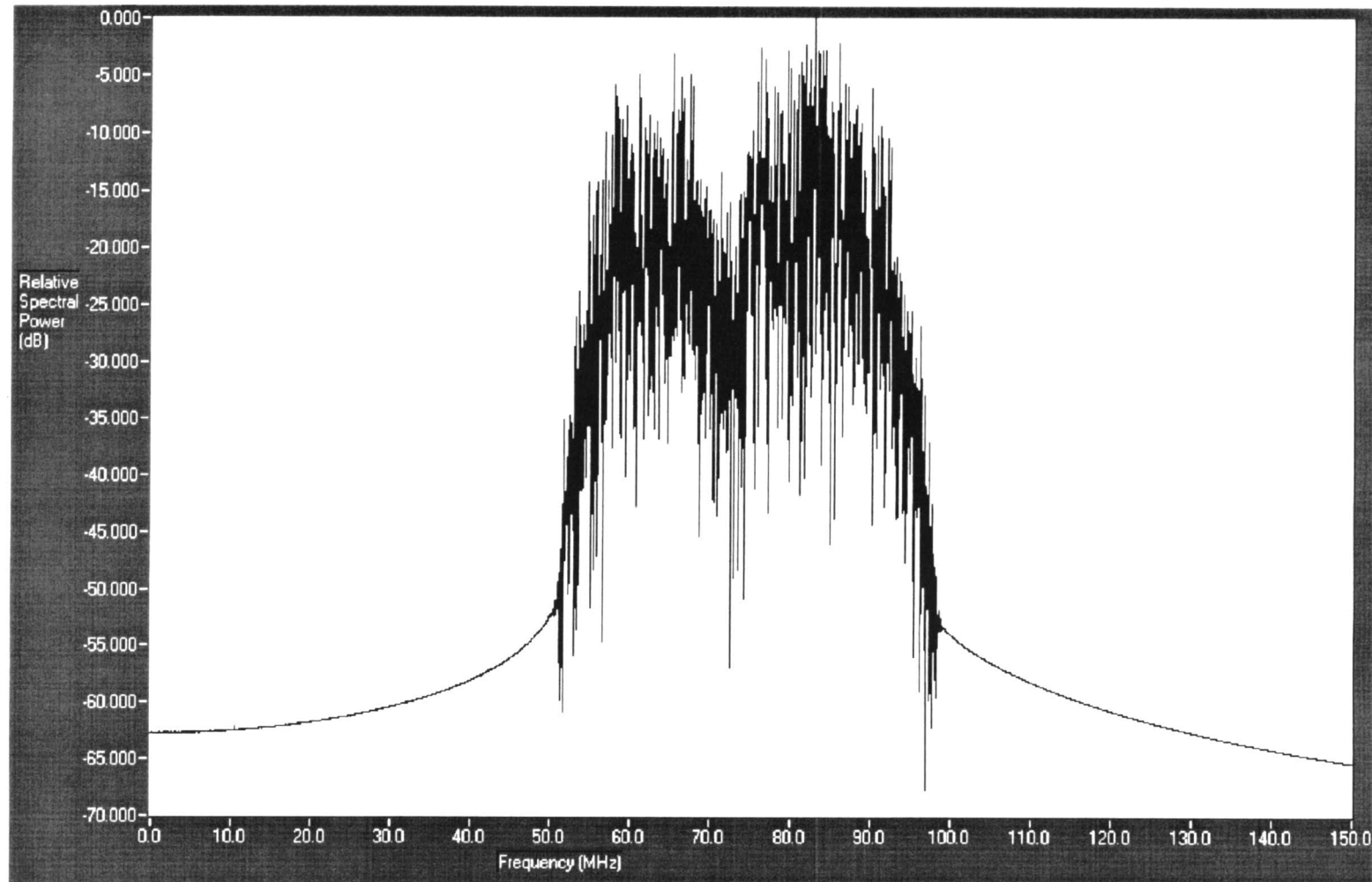
Constellation Before Equalization



Constellation After Equalization



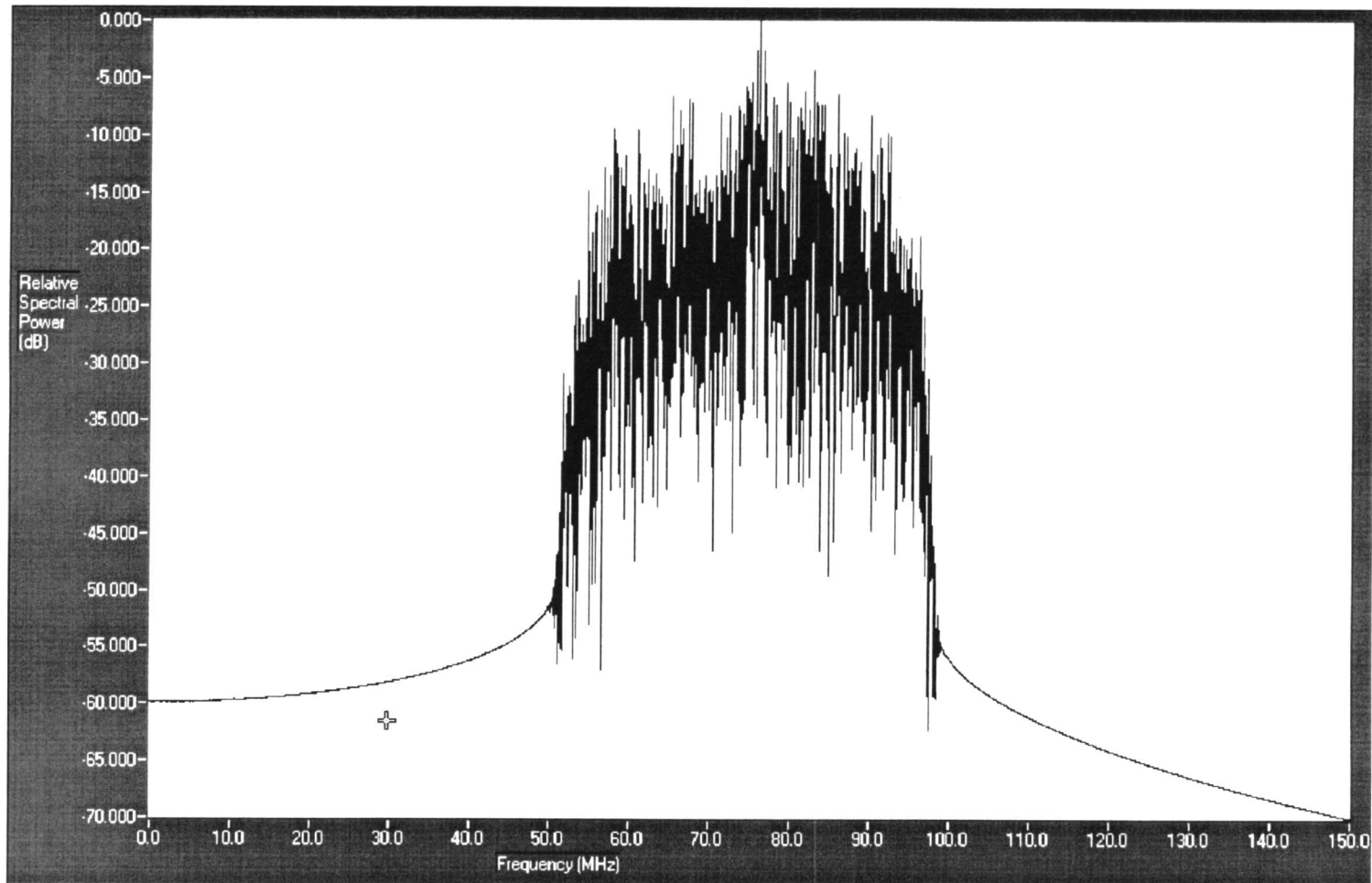
Spectrum Before Equalization



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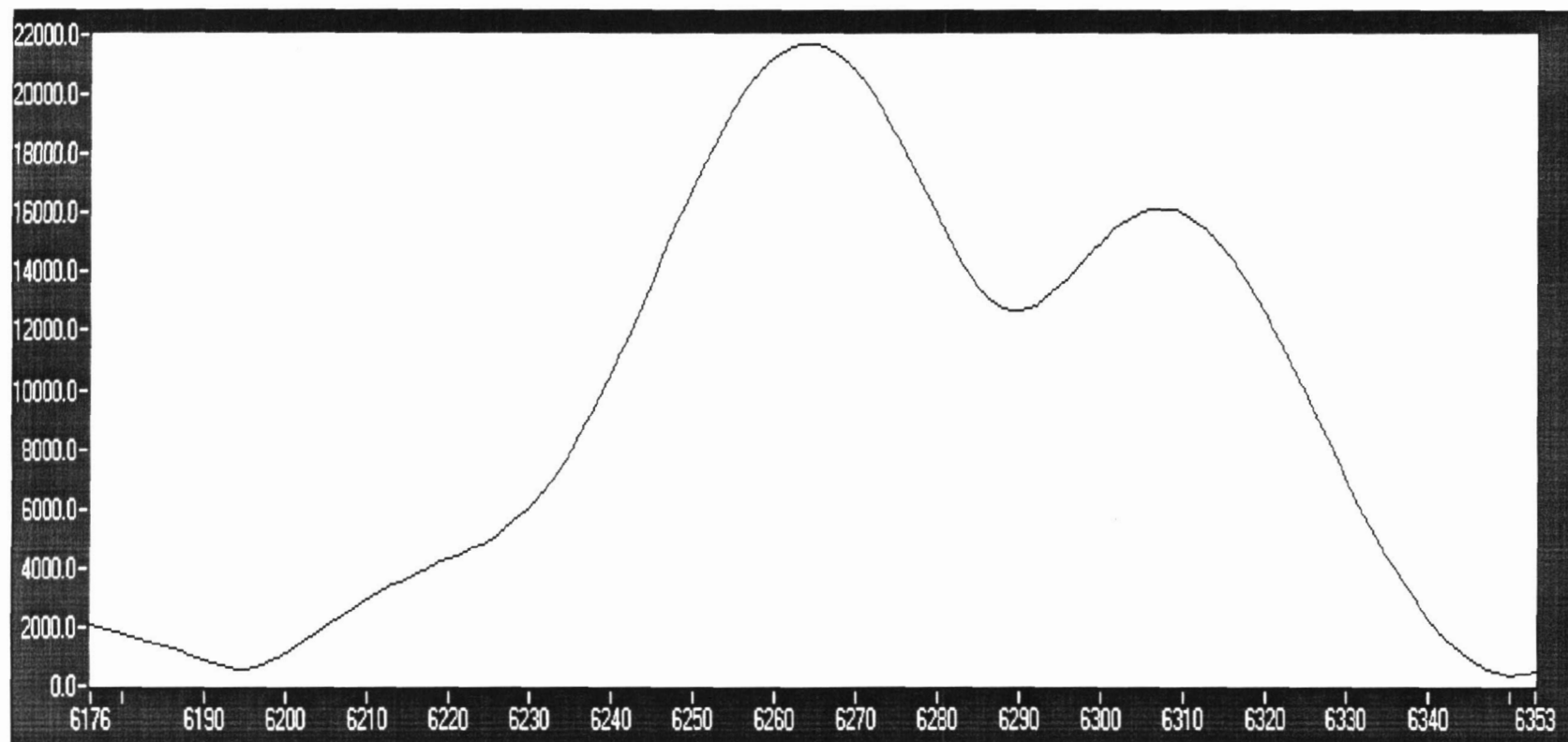
Spectrum After Equalization



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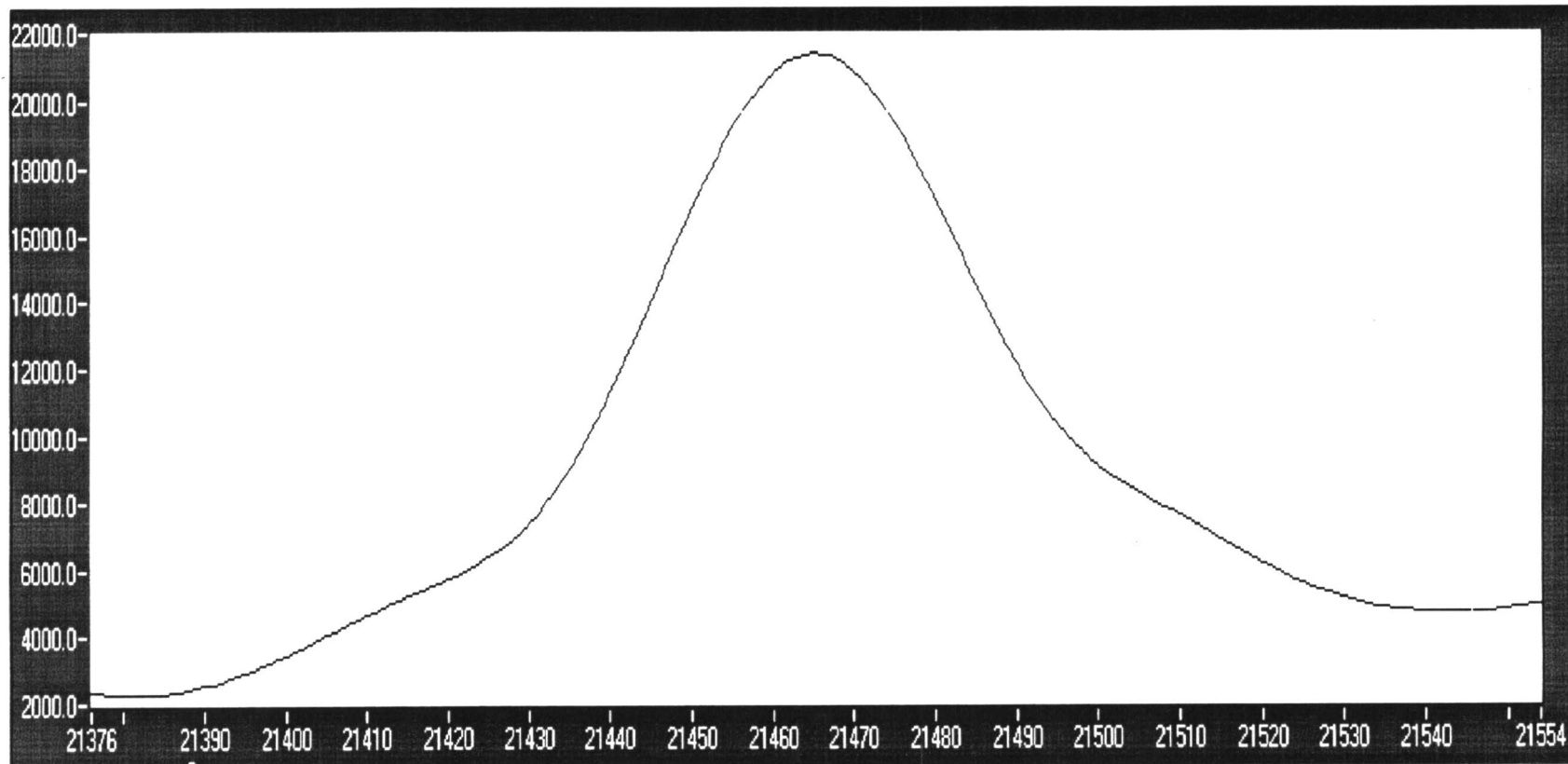
Trigger Response Before Equalization



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Trigger Response After Equalization



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OTHER TESTS

Lighthouse to boat

Hurricane Point across bay to Lighthouse

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Equalization

In almost all cases multipath could be modeled as 2-ray

Successfully equalized by processing the received signal complex envelope, $s_k = I_k + jQ_k$
with a single delay recursive filter, $\frac{1}{1 + Ae^{jP}z^{-(D+1)}}$

Where

A is the fractional amplitude of the 2nd multi-path signal relative to LOS signal

P is the relative angle,

D is the relative delay-1

In the rare cases where the reflected ray is larger than the incident ray
The open form of the above equation must be used

Additional iteration of single delay compensation resulted in further improvement
even though ideally parameters for all delays would be searched simultaneously

Test Results

Aircraft to Boat

No significant problems

No significant satellite radio interference

Some flat fading detected

Occasional frequency dependent fading: from ship's mast



Test Results

Aircraft to Lighthouse

Frequency Dependent Fading

Severe in-band satellite radio interference

Most data unusable due to interference



HERT's Objective

To measure time of arrival with precisely located shock sensors in an "in flight high explosive system" and send that information by radio link to a receiving station.

HERT is a measurement system, not just some sensors

Cooperative efforts:

Partner with Honeywell, Kansas City Plant

Work closely with Sandia and

Lawrence Livermore National Labs

Extensively tested from 1995 to present:

Non-Explosive Radio Frequency Ground Tests

Explosive Ground Tests

RF and Telemetry System

Sensor Systems

Flight Test Vandenberg to Kwajalein

Telemetry System

Flight Survival

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HERT Transmitter Implementation

100Mbit/sec raw data rate

40nS symbol period

Pulse mode of transmission

Fast switching linear amplifier

Embedded parity error encoding

FPGA controlled I-Q modulation

HERT's General Features and Parameters

Time of arrival measurement for
64 Channels, 10 ns resolution

Optical base sensor inputs

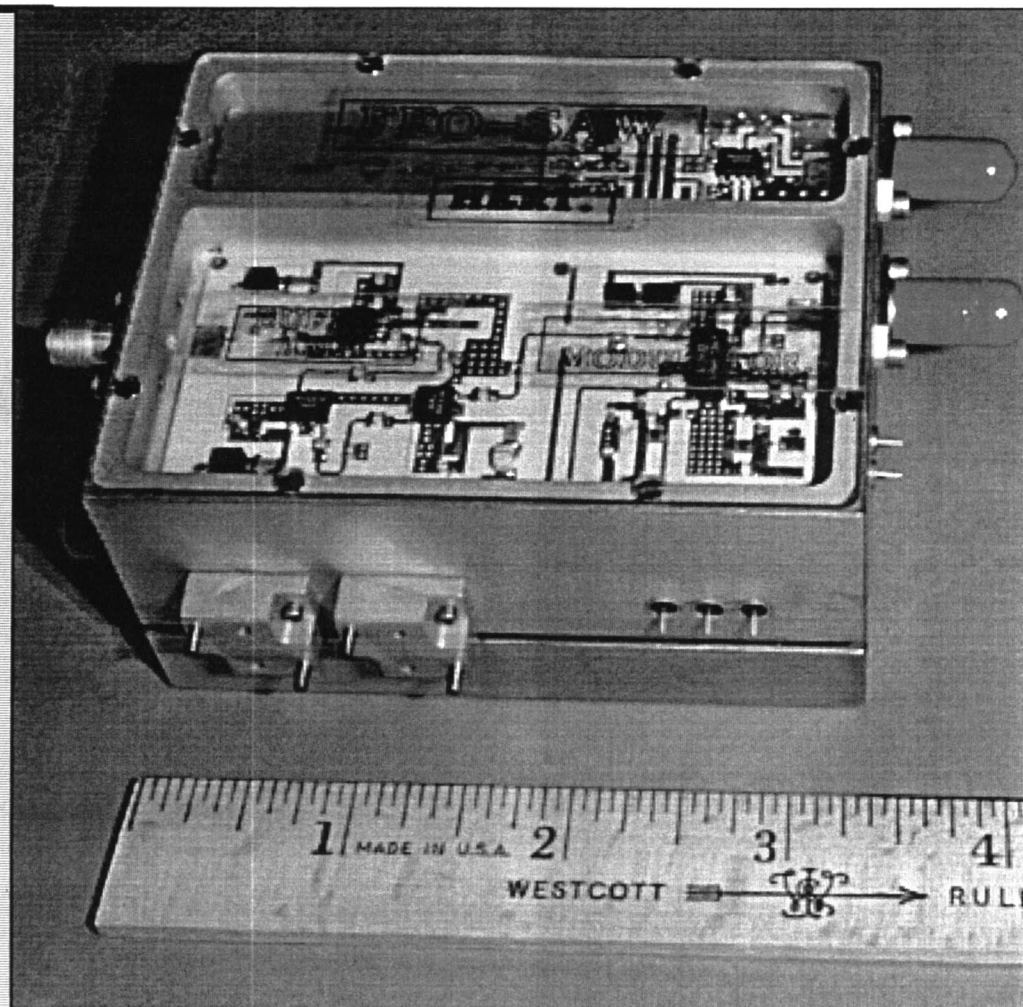
Simultaneous or time separated
measurements; 10ns to 160 • s

Small size 1.75 x 2.5 x 3.5 inches

Lightweight 1.25 lbs

Electrically efficient 5 watts

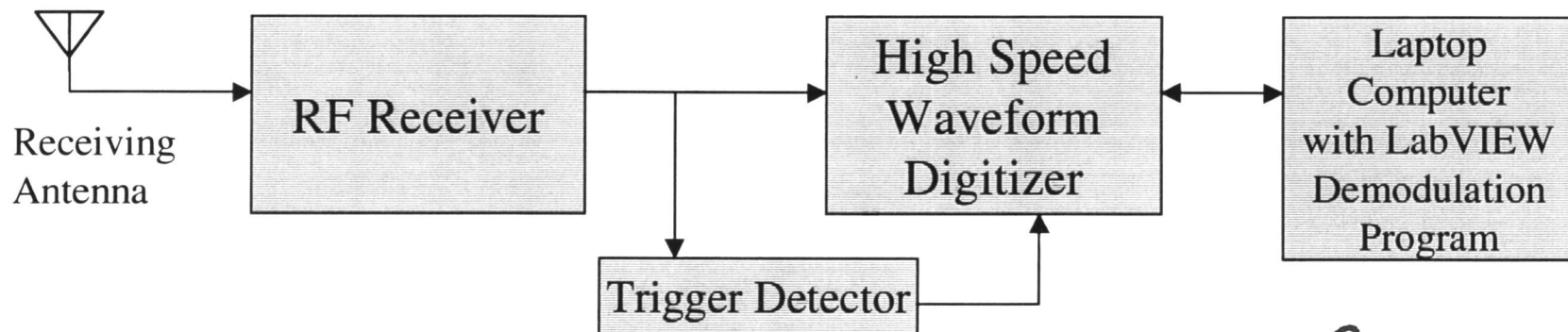
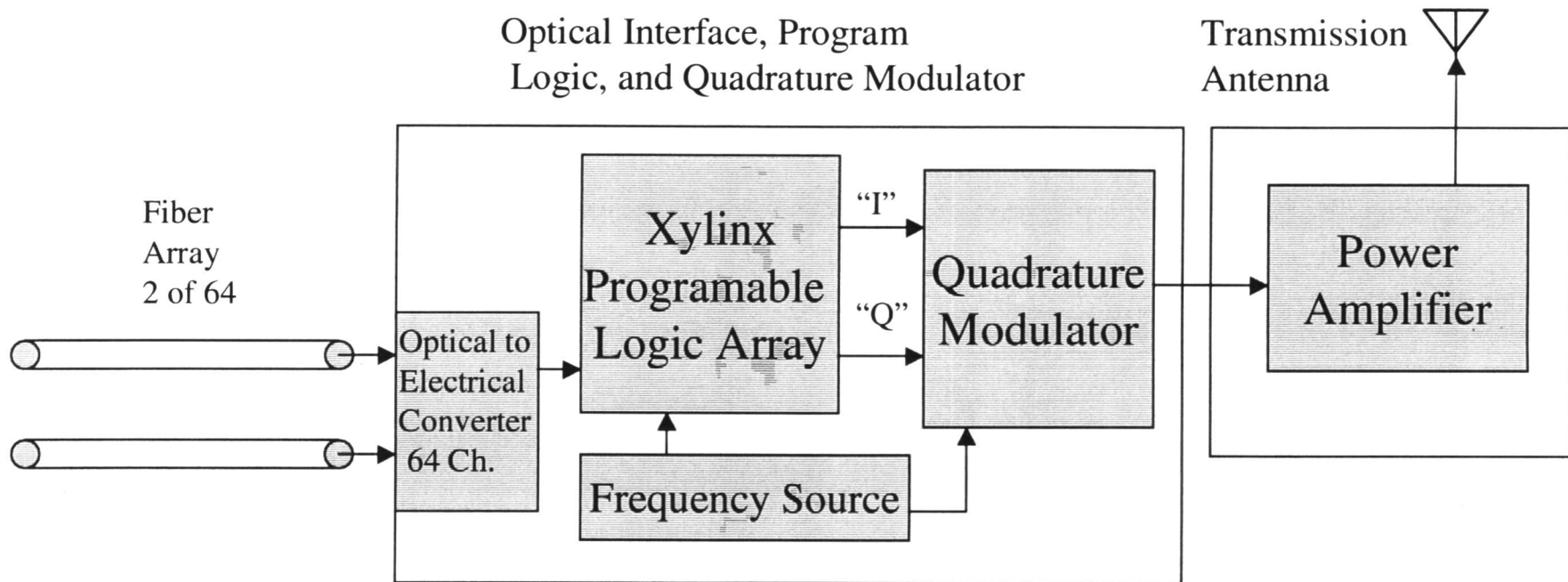
Operates in a BURST mode for
efficient use of electrical
power



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HERT System Basic Block Diagram



HERT Systems

Sensors

Self-Check

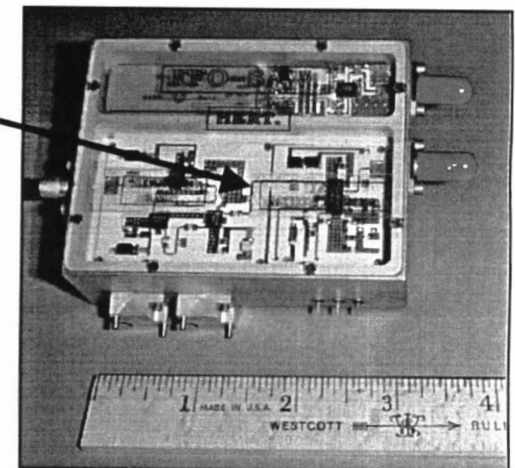
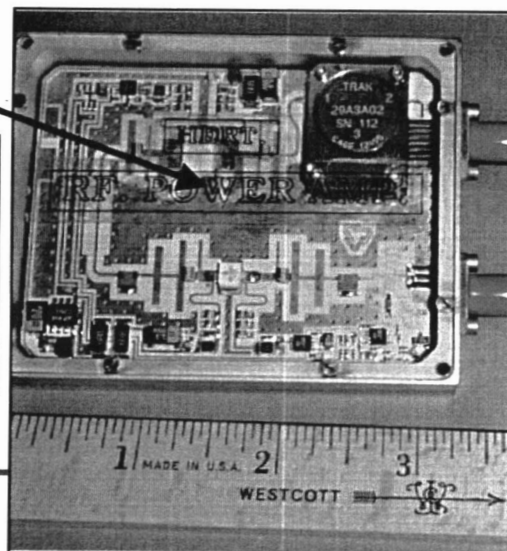
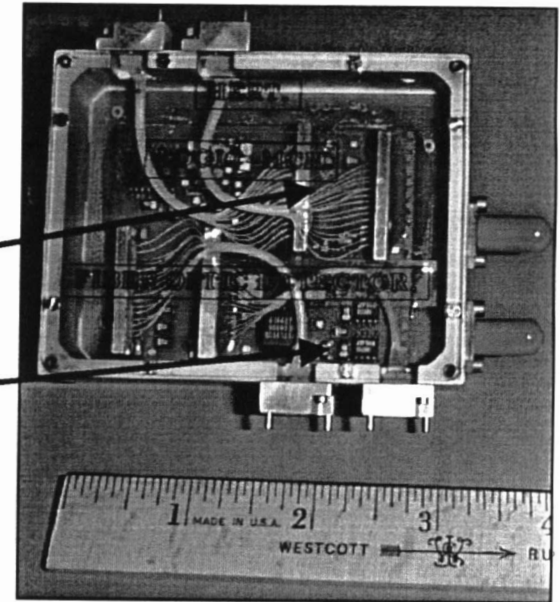
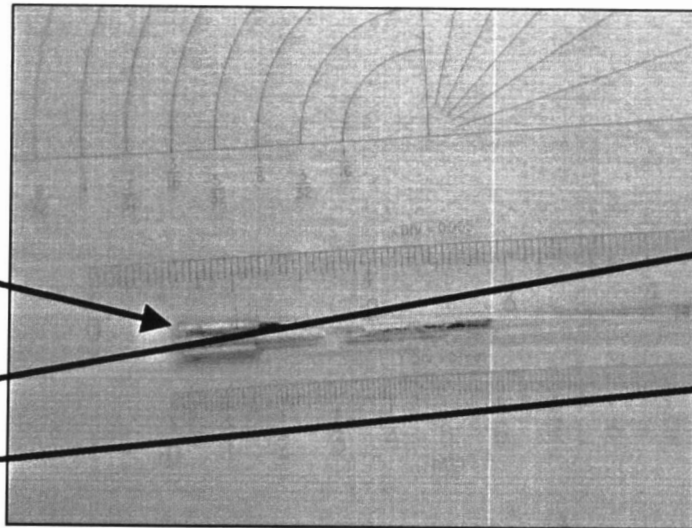
Optical Detector

Logic

Radio Frequency (RF) and Modulation

Power Amplifier

Ground Station and Receiver



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Logic

Specifications and Features

100 MHz Xylinx PLA

Starts on arrival of first signal

10 ns detection of "Time
of Arrival" for the
64 optical inputs

Formats Channel #, Arrival time,
and sequence of arrival
for the 64 channels

Converts data into digital QAM-16
format

Generates unique digital trigger
word

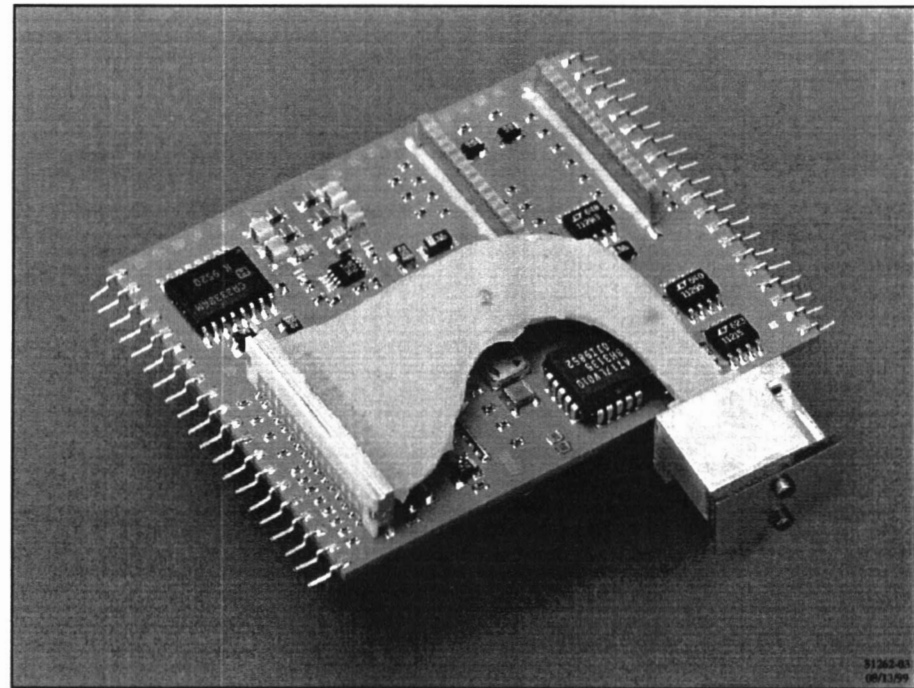
Completes one cycle of transmission
in about 16 μ s

Multi-Chip-Module (MCM)

1 x 16 MT Fiber connector

1 x 16 Fiber Array

1 x 16 Optical to Electrical
Convert Modules



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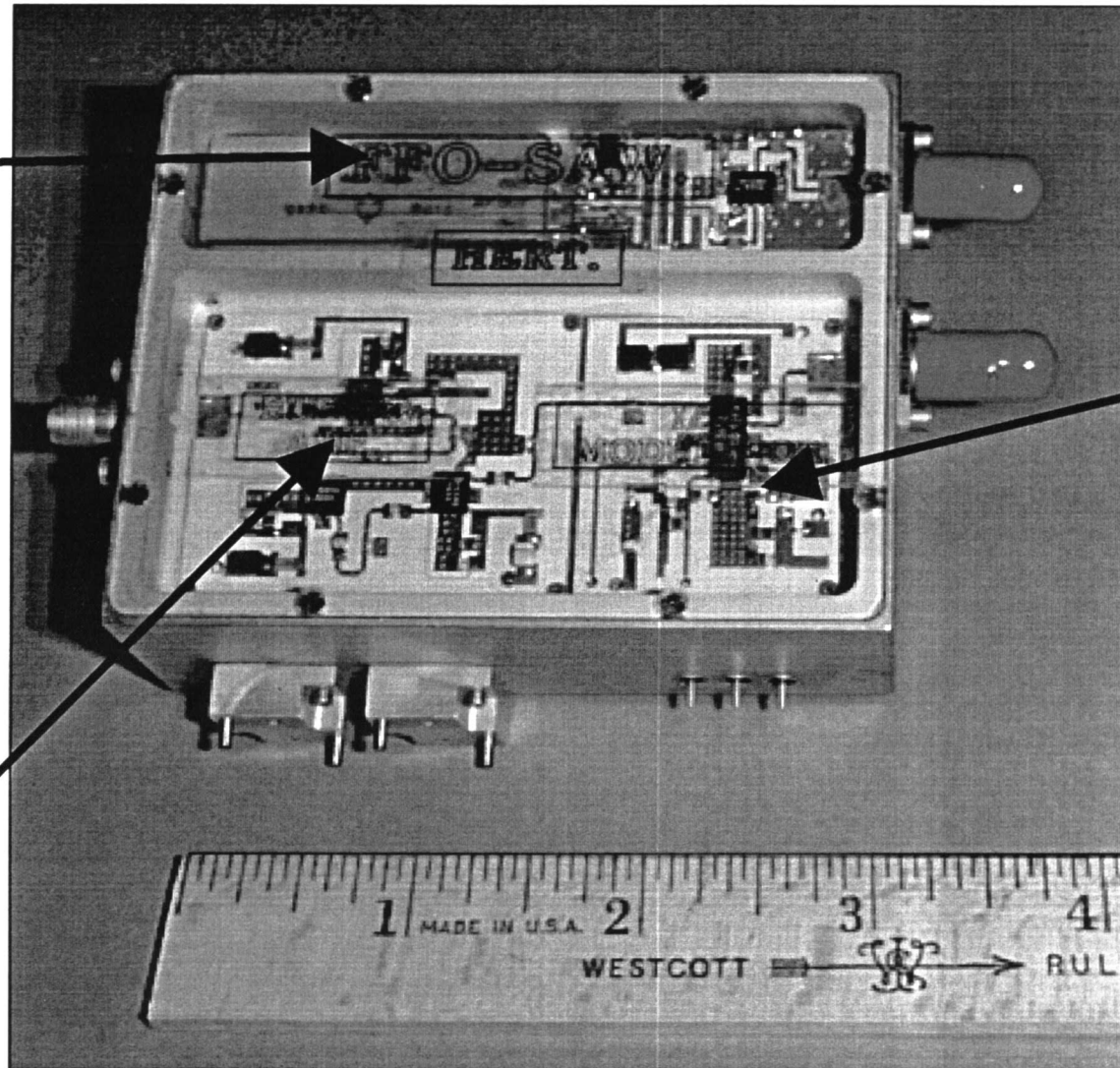
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Radio Frequency and Modulation

Adjustable
Surface
Acoustic
Wave
Oscillator
(SAW)
2.2 to 2.4
GHz
Flight Rugged

Buffer Amp
0.1 watt
output

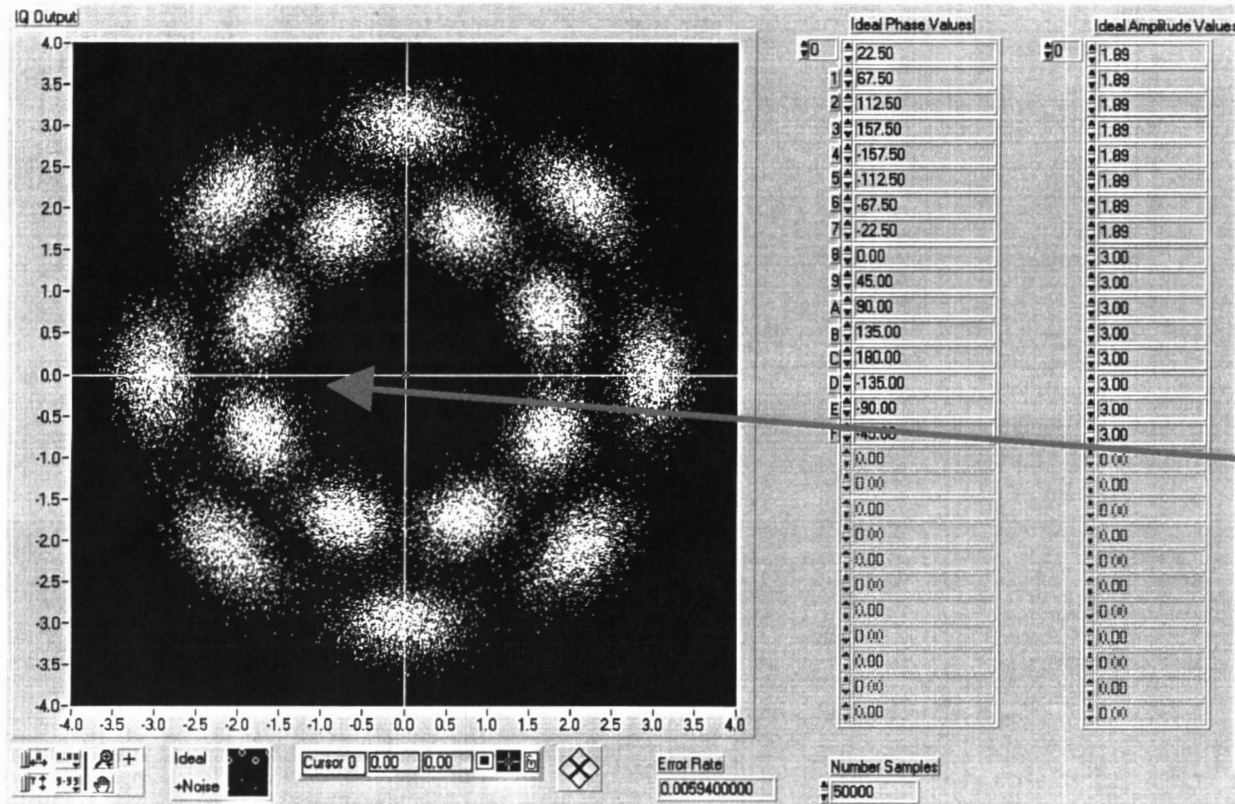
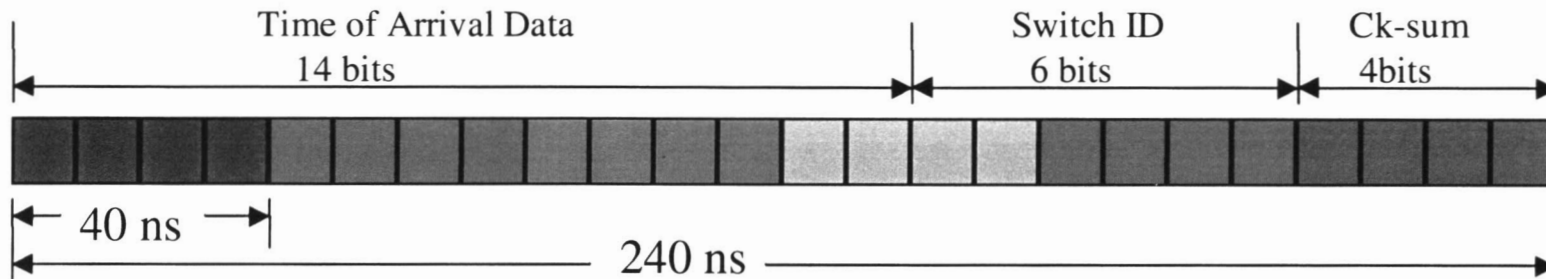
Quadrature
Amplitude
Modulator
16 State
(QAM-16)



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Radio Frequency and Modulation



QAM-16 gives 4 to 1 data compression and reduces transmission time from 64 us to 16 us

Each spot represents a 4 bit hexadecimal word
1 = 1, 3 = 3, 10 = A, etc.

Data is represented by changes in Amplitude and Phase from one hex word to another hex word

Novel Modulation Method

Differential-Phase / Absolute-Amplitude / Two-Level Polar / 16QAM

Advantages:

- 1. Less backoff needed than with rectangular QAM - 3dB works well**
- 2. Allows coherent or non-coherent demodulation**
- 3. Simple FPGA transmitter encoding algorithm**
- 4. Spectrally efficient**
- 5. High Data Rate**

Power Amplifier

Specifications and Features
Class A, Linear Operation

RF power out: 10 watts

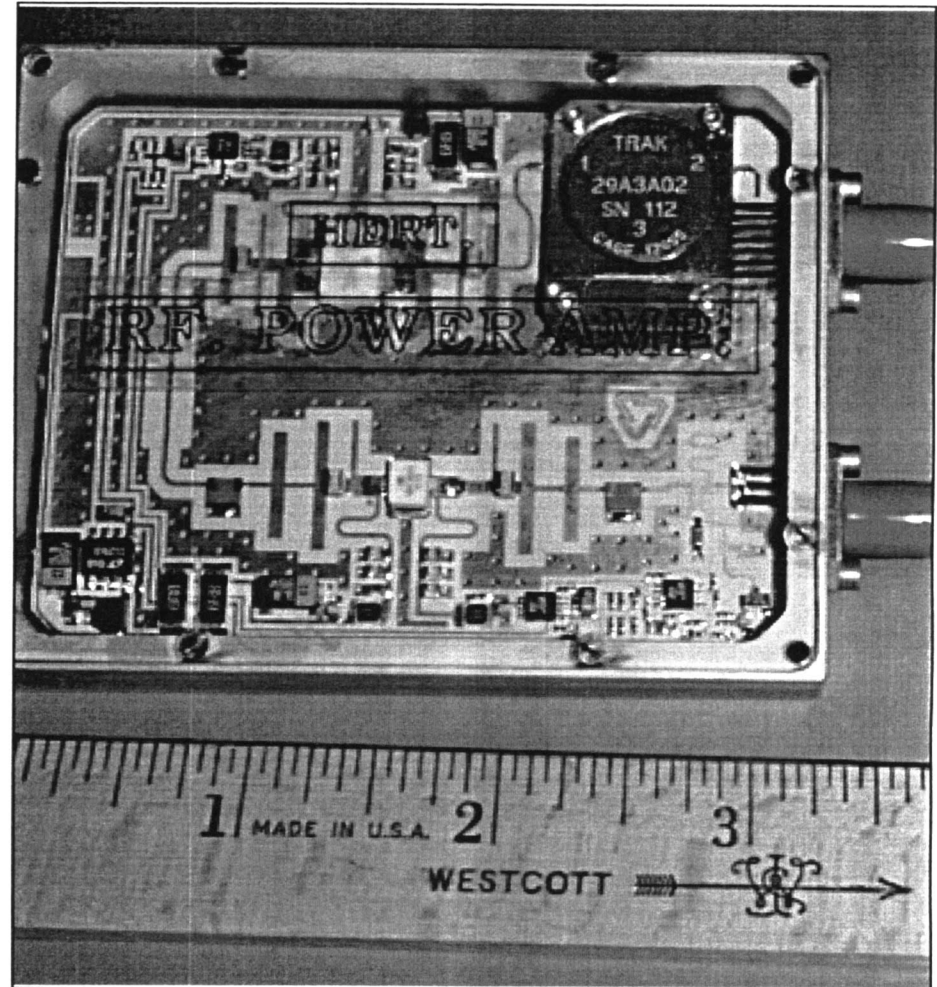
Frequency: 2.2 to 2.4 GHz

Efficiency: About 20%

On only when the RF
burst from the Logic
and Modulator is Present

Small in size, low weight

Configured with HERT or can
be moved



Honeywell

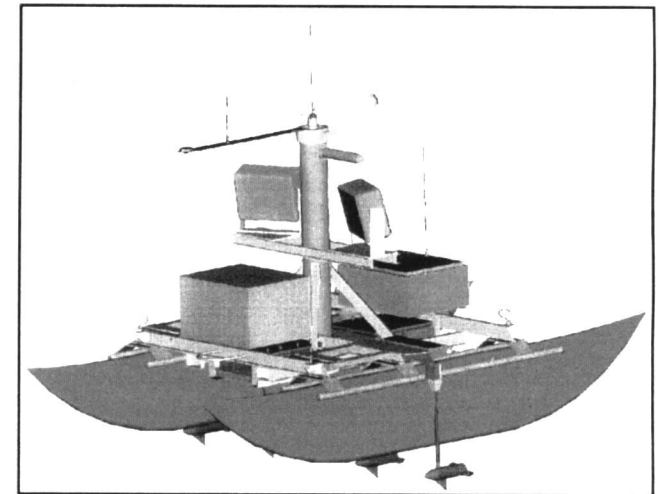
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Receiving Station Capabilities

Land-base with existing antennas and telemetry equipment

Sea-based on station keeping rafts

Air-based on telemetry receiving airplanes



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Conclusions

Ocean multi-path can usually be modeled as 2-ray and can be equalized with a single delay recursive filter, or its non-recursive equivalent when main is weaker than the delayed ray

Although not ideal, additional improvement can be obtained by additional independent iterations of 2-ray compensation.

Adequate optimization criteria for equalization are the “constellation spread” and “correlation of correlation”.

HERT telemetry signals can usually be recovered even under most severe multipath conditions.

